# Planning a finite time transition from a non-stationary to a stationary point without overshoot

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*Abstract*— The problem of planning a finite time transition of a trajectory from a non-stationary point to a stationary setpoint is addressed. As opposed to standard approaches, where the transition functions are polynomials, the specific choice of non-analytic function proposed may easily be trimmed to show no overshoot and only an adjustable undershoot during transition. The main result is a recursive formula for a simple parametrization of the transition function, as needed in tracking problems. Two examples underscore the ease of the approach.

## I. INTRODUCTION

Consider the problem of planning the transition of a time function y(t) on a finite time interval  $t \in [t_1, t_2]$ . Let  $t = t_1$ be the time associated with r left boundary conditions (BC)

$$y^{(i)}(t_1) := \left. \frac{d^i y}{dt^i} \right|_{t=t_1} = \underline{y}_i, \quad i = 0, 1, \dots, r-1.$$
(1)

Correspondingly, at  $t = t_2$  let y(t) satisfy r right BC

$$y^{(i)}(t_2) := \left. \frac{d^i y}{dt^i} \right|_{t=t_2} = \overline{y}_i, \quad i = 0, 1, \dots, r-1.$$
 (2)

A straight-forward idea for tackling this problem is to use polynomials for meeting the 2r BC of (1) and (2). The least degree polynomial shows degree 2r-1 and is uniquely determined by the BC. Polynomials with degrees larger than 2r-1that meet the BC may be found, as well. Various approaches of polynomial kind are exposed in [8], for example. An approximate optimization-based approach presents [4]. For the planning of transitions between stationary points see [5], where a simple to use formula for the transition polynomial is given. An input shaping approach by means of polynomials with additional exponential decay is derived in [7]. Recently, trajectory generation received attention within the different inversion-based approaches to the control of systems with internal dynamics [1], [2], [6], [3].

In this paper, let the task be confined to the planning of the transition from a non-stationary point of y(t), as specified in (1), to a stationary point as given by the right BC

$$y(t_2) = \overline{y}_0, \quad y^{(i)}(t_2) = 0, \ i = 1, \dots, r-1,$$
 (3)

being a special case of the right BC (2).

It turns out that in the case of planning from non-stationary to stationary points there are decisive drawbacks when employing polynomials: Primarily, there is no a priori criterion to decide whether the transition polynomial resulting from the BC in (1) and (2) will show an overshoot or undershoot.

\* J. Reger is postdoc with the Systems and Control Theory Group, Max Planck Institute for Dynamics of Complex Technical Systems, Sandtorstr. 1, D-39106 Magdeburg, Germany (email: reger@ieee.org) Standard methods as calculating the set of zeroes with respect to the polynomial's first time derivative give a posteriori insight, only. Secondly, it is a well-known fact that large absolute values of  $\underline{y}_i$  and  $\overline{y}_i$  give rise to polynomials with very large degree, accompanied by the problem of a wavy transition in course of time.

Hence, the proposal of this paper is to refrain from polynomials, and rather employ a particular non-analytic function. A formula for the recursive parametrization of this function is provided that may easily be trimmed to show no overshoot and just a reduced undershoot when adjusting one single parameter.

The paper is organized as follows: Section II contains the derivation of the parametrization of a non-analytic function, adequate for solving the above-stated transition problem on a unity time interval. Section III provides the main result that holds for arbitrary time intervals. The paper ends with a discussion and some examples in Section IV.

## II. PARAMETRIZATION OF A NON-ANALYTIC TRANSITION FUNCTION

Consider the transition function

$$y(t) = \left(c_0 + c_1 t + \dots + c_{r-1} t^{r-1}\right) e^{\frac{-1}{(t-1)^n}} + \overline{y}_0 \qquad (4)$$

with even exponent  $n \in \{2, 4, 6, ...\}$  and real coefficients  $c_i$ , i = 0, 1, ..., r - 1. It is not difficult to show that the ansatz (4) satisfies the stationary right BC (3) in a limit sense

$$\lim_{t \to 1} y(t) = \overline{y}_0 \quad \text{and} \quad \lim_{t \to 1} y^{(i)}(t) = 0, \ i = 1, 2, \dots$$
(5)

which implies that y(t) given in (4) is non-analytic at t = 1.

The coefficients  $c_i$  serve to satisfy the left BC (1) at the time instant  $t_1 = 0$ . In a next step, the result to be obtained at time instants  $t_1 = 0$  and  $t_2 = 1$  may then be generalized to arbitrary instants of time  $t_1 < t_2$ ,  $t_1, t_2 \in \mathbb{R}$ .

In view of the left BC (1), the coefficients  $c_i$  may be determined by equating  $y^{(i)}(0) = \underline{y}_i$ ,  $i = 0, 1, \ldots, r-1$ .

In the first place, observe that

,

$$y(0) = c_0 e^{\frac{-1}{(-1)^n}} + \overline{y}_0 \stackrel{!}{=} \underbrace{y}_0 \Rightarrow c_0 = (\underbrace{y}_0 - \overline{y}_0) e \,. \tag{6}$$

Thereafter, for i = 1, 2, ... determine the *i*-th time derivative

$$y^{(i)}(t) = \sum_{\nu=0}^{i} {i \choose \nu} \left( \frac{d^{i-\nu}}{dt^{i-\nu}} \sum_{\mu=0}^{r-1} c_{\mu} t^{\mu} \right) \left( \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{(t-1)^{n}}} \right)$$
$$= \sum_{\nu=0}^{i} {i \choose \nu} \left( \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{(t-1)^{n}}} \right) \sum_{\mu=i-\nu}^{r-1} c_{\mu} \frac{d^{i-\nu}}{dt^{i-\nu}} t^{\mu}$$
$$= \sum_{\nu=0}^{i} {i \choose \nu} \left( \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{(t-1)^{n}}} \right) \sum_{\mu=i-\nu}^{r-1} \frac{\mu!}{(\mu+\nu-i)!} c_{\mu} t^{\mu+\nu-i}$$
(7)

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and for adaption to the left BC (1), for any i = 1, 2, ..., r-1at  $t_1 = 0$  we have to require that

$$\underline{y}_{i} \stackrel{!}{=} \lim_{t \to 0} y^{(i)}(t) = \sum_{\nu=0}^{i} {i \choose \nu} \left( \lim_{t \to 0} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{(t-1)^{n}}} \right) \\
\sum_{\mu=i-\nu}^{r-1} \frac{\mu!}{(\mu+\nu-i)!} c_{\mu} \left( \lim_{t \to 0} t^{\mu+\nu-i} \right) \\
= \sum_{\nu=0}^{i} {i \choose \nu} \left( \lim_{t \to 0} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{(t-1)^{n}}} \right) (i-\nu)! c_{i-\nu} \\
= \sum_{\nu=0}^{i} \frac{i!}{\nu!} c_{i-\nu} \left( \lim_{t \to -1} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{t^{n}}} \right)$$
(8)

which together with equation (6) is a linear system of equations that allows to solve for the r unknown coefficients  $c_i$  in terms of the BC  $\underline{y}_i$ , i = 0, 1, ..., r - 1, in a unique way.

The triangular structure of equation (8) suggests to exploit a simple recurrence scheme. Indeed, rewriting (8) yields

$$\underline{y}_{i} = i! c_{i} \left( \lim_{t \to -1} e^{\frac{-1}{t^{n}}} \right) + \sum_{\nu=1}^{i} \frac{i!}{\nu!} c_{i-\nu} \left( \lim_{t \to -1} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{t^{n}}} \right) \\
= \frac{i!}{e} c_{i} + \sum_{\nu=1}^{i} \frac{i!}{\nu!} c_{i-\nu} \left( \lim_{t \to -1} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{t^{n}}} \right).$$
(9)

Thus, with (6) we derive the recurrence (i = 0, 1, ..., r - 1)

$$c_{i} = e\left(\frac{\underline{y}_{i}}{i!} - \sum_{\nu=1}^{i} \frac{c_{i-\nu}}{\nu!} \lim_{t \to -1} \frac{d^{\nu}}{dt^{\nu}} e^{\frac{-1}{t^{n}}}\right), c_{0} = (\underline{y}_{0} - \overline{y}_{0}) e.$$
(10)

The derivatives on the right hand side of (10) may be evaluated further. To this end, use the chain rule

$$\frac{df(t)}{dt} = f(t)\frac{dg(t)}{dt}, \quad f(t) = e^{g(t)}, \ g(t) = \frac{-1}{t^n}.$$
 (11)

In doing so, we may refer to Leibniz' rule for differentiating products again, hence

$$f^{(\nu+1)}(t) = \sum_{i=0}^{\nu} {\nu \choose i} \left(\frac{d^{\nu-i}}{dt^{\nu-i}} f(t)\right) \left(\frac{d^{i+1}}{dt^{i+1}} g(t)\right)$$
(12)

and shifting  $\nu \rightarrow \nu - 1$  it follows that

$$f^{(\nu)}(t) = \sum_{i=0}^{\nu-1} {\nu-1 \choose i} f^{(\nu-i-1)}(t) g^{(i+1)}(t), \quad \nu = 1, 2, \dots$$
(13)

where the  $\nu$ -th time derivative of f(t) is expressed in terms of lower order derivatives in form of a recurrence. Finally, recalling (11) it remains to evaluate

$$g^{(i+1)}(t) = \frac{d^{i+1}}{dt^{i+1}} \left(\frac{-1}{t^n}\right) = (-1)\frac{d^{i+1}}{dt^{i+1}}t^{-n}$$
$$= (-1)(-n)(-n-1)(-n-2)\cdots(-n-i)\frac{1}{t^{n+i+1}}$$
$$= (-1)^i \frac{(n+i)!}{(n-1)!}\frac{1}{t^{n+i+1}}.$$
 (14)

A consequence is the recurrence

$$f^{(\nu)}(t) = \sum_{i=0}^{\nu-1} {\nu-1 \choose i} \frac{(n+i)!}{(n-1)!} \frac{(-1)^i}{t^{n+i+1}} f^{(\nu-i-1)}(t)$$
  
$$f^{(0)}(t) = e^{\frac{-1}{t^n}}$$
(15)

which at t = -1 yields

$$f^{(\nu)}(-1) = \sum_{i=0}^{\nu-1} {\nu-1 \choose i} \frac{(n+i)!}{(n-1)!} (-1)^{n+1} f^{(\nu-i-1)}(-1)$$
  
$$f^{(0)}(-1) = 1/e$$
(16)

to be solved until index  $\nu = r - 1$ , as indicated by (10).

#### III. MAIN RESULT

Simple steps of manipulation show that a possible transition function, which satisfies the 2r BC of (1) and (3) at arbitrary instants of time  $t_1$  and  $t_2$ , reads

$$y(t) = \underline{y}_0 + (1/e)^{\left(\frac{t_2 - t_1}{t_2 - t}\right)^n} \sum_{i=0}^{r-1} c_i \left(\frac{t - t_1}{t_2 - t_1}\right)^i$$
(17)

with coefficients  $c_i$  that result from the recurrence

$$c_{i} = e\left(\frac{\underline{y}_{i}(t_{2}-t_{1})^{i}}{i!} - \sum_{\nu=1}^{i} \frac{c_{i-\nu}}{\nu!} f^{(\nu)}(-1)\right)$$
(18)  
$$c_{0} = (\underline{y}_{0} - \overline{y}_{0}) e.$$
(19)

where the values of  $f^{(\nu)}(-1)$  follow from (16).

## IV. DISCUSSION AND EXAMPLES

In order to find a minimal parameter  $n = n_{\min}$  subject to which no overshoot occurs for  $t \in (t_1, t_2)$ , note that with the coefficients  $c_i$  determined as above, the necessary condition  $\frac{d}{dt}y(t) = 0$  for an extremal point may be written as

$$\sum_{i=0}^{r-1} c_i \left(t - t_1\right)^i \left(t_2 - t_1\right)^{r-1-i} \times \left(i \left(t_2 - t\right)^{n+1} - n \left(t_2 - t_1\right)^n \left(t - t_1\right)\right) = 0.$$
 (20)

In the main, two cases need to be distinguished:

- 1) When increasing *n* starting from 2, given the bottomup-transition  $\underline{y}_0 < \overline{y}_0$  and  $\underline{y}_1 > 0$  (top-down-transition  $\underline{y}_0 > \overline{y}_0$  and  $\underline{y}_1 < 0$ ), then  $n_{\min}$  is the first number for which the polynomial in (20) shows no zeroes in  $(t_1, t_2)$ . Thus, the overshoot as depicted in the plots of Figure 1 can be avoided by increasing *n*.
- 2) When increasing *n* starting from 2, given the bottomup-transition  $\underline{y}_0 < \overline{y}_0$  and  $\underline{y}_1 < 0$  (top-down-transition  $\underline{y}_0 > \overline{y}_0$  and  $\underline{y}_1 > 0$ ), then  $n_{\min}$  is the first number for which the polynomial in (20) shows one single zero in  $(t_1, t_2)$ . In this case, besides avoiding an overshoot, one may additionally reduce the undershoot by a further increase of the parameter *n* until the undershoot falls below a specified bound, as shown in the lower plots of Figure 1 (see arrows).

## TABLE I

LEFT BC FOR THE PARAMETRIZATION OF THE TRANSITION FUNCTION (17) AS DEPICTED IN FIGURE 2 AND FIGURE 3

left BC	$\underline{y}_0$	$\underline{y}_1$	$\underline{y}_2$	$\underline{y}_3$	$\underline{y}_4$
Figure 1	0	20	30	60	40
Figure 2	0	-15	200	100	40

Either of these cases is demonstrated resorting to an example transition from  $t_1 = 0$  to  $t_2 = 2$  subject to r = 5 non-stationary BC at  $t = t_1$  (see Table I). A stationary value of  $\overline{y}_0 = 10$  shall be reached for both transitions at  $t = t_2$ .

Case 1 is illustrated in Figure 2: A calculation of the corresponding zeroes of (20) for n = 2, 4, 6, ..., 16 yields that  $n_{\min} = 8$ , where no overshoot takes place, anymore. An increase of n further accelerates the response.

Case 2 is illustrated in Figure 3: A calculation of the corresponding zeroes of (20) for n = 2, 4, 6, ..., 16 yields that  $n_{\min} = 6$ , where no overshoot takes place, anymore. A further increase of n helps accelerate the response and further reduces the undershoot. Such transitions resemble behaviors that are typical within the tracking of non-minimum phase systems.



Fig. 1. Dependency of overshoot and undershoot on left side boundary conditions—by increasing n in the non-analytic transition (17) the depicted overshoots may be avoided and the undershoots (marked with arrow) are reduced

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Fig. 2. Case 1: transition function (17) for left BC according to Table I; n = 2 (black line), n = 4 (red line), n = 6 (blue line); for n = 8 (green line) no overshoot occurs anymore; thin black lines show faster response when increasing n (plotted are n = 10, 12, 14, 16)



Fig. 3. Case 2: transition function (17) for left BC according to Table I; n = 2 (black line), n = 4 (red line); for n = 6 (green line) no overshoot occurs anymore; increasing *n* helps reduce the undershoot further (plotted are n = 8, 10, 12, 14, 16)

#### REFERENCES

- D. Chen and B. Paden, Stable Inversion of Nonlinear Non-Minimum Phase Systems, *International Journal of Control*, vol. 64, no. 1, pp. 81–97, 1996
- [2] S. Devasia, D. Chen, and B. Paden, Nonlinear Inversion-Based Output Tracking, *IEEE Transactions on Automatic Control*, vol. 41, no. 7, pp. 930–942, 1996
- [3] K. Graichen, V. Hagenmeyer, and M. Zeitz, A New Approach to Inversion-Based Feedforward Control Design for Nonlinear Systems, *Automatica*, vol. 41, no. 12, pp. 2033–2041, 2005
- [4] M. van Nieuwstadt and R. Murray, "Approximate Trajectory Generation for Differentially Flat Systems with Zero Dynamics", 34th IEEE Conference on Decision and Control, vol. 4., pp. 4224-4230, New Orleans, USA, 1995
- [5] A. Piazzi and A. Visioli, Optimal Noncausal Set-Point Regulation of Scalar Systems, *Automatica*, vol. 37, no. 1, pp. 121–127, 2001
- [6] A. Piazzi and A. Visioli, Optimal Inversion-Based Control for the Set-Point Regulation of Nonminimum-Phase Uncertain Scalar Systems, *IEEE Transactions on Automatic Control*, vol. 46, no. 10, pp. 1654– 1659, 2001
- [7] M. Sahinkaya, Input shaping for vibration-free positioning of flexible systems, *Proc. Instn. Mech. Engrs.*, vol. 215, part I, pp. 467–481, 2001
- [8] H. Sira Ramírez and S. Agrawal, *Differentially Flat Systems*, Marcel Dekker, 2004