



Subspace Identification of a Distillation Column

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Outline

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Background

◆ State-space models

- convenient for MIMO systems
- problems with time delays

$$x(t+1) = Ax(t) + Bu(t) + Ke(t)$$

$$y(t) = Cx(t) + Du(t) + e(t)$$

◆ Identification by PE methods

- minimize $V_N(\theta) = \frac{1}{N} \sum_{t=0}^{N-1} \|\varepsilon(t, \theta)\|^2$ with respect to θ subject to

$$\hat{x}(t+1, \theta) = [A(\theta) - K(\theta)C]\hat{x}(t, \theta) + B(\theta)u(t) + K(\theta)y(t)$$

$$\varepsilon(t, \theta) = y(t) - C\hat{x}(t, \theta) - D(\theta)u(t)$$

- nonlinear iterative optimization, usually ill-conditioned
- local minima
- choice of model structure is problematic

⇒ PE methods have **inherent difficulties for MIMO systems** (Katayama, 2005).

Basic Idea of Subspace Identification

- ◆ Determine (A, B, C, D) directly from data through algebraic manipulations — i.e., no iterative optimization
 - If the state vector $\tilde{x}(t)$ can be estimated, (A, B, C, D) is obtained by

$$\begin{bmatrix} \hat{A} & \hat{B} \\ \hat{C} & \hat{D} \end{bmatrix} = \left(\sum_{t=0}^{N-1} \begin{bmatrix} \tilde{x}(t+1) \\ y(t) \end{bmatrix} \begin{bmatrix} \tilde{x}(t+1) \\ y(t) \end{bmatrix}^T \right) \left(\sum_{t=0}^{N-1} \begin{bmatrix} \tilde{x}(t) \\ u(t) \end{bmatrix} \begin{bmatrix} \tilde{x}(t) \\ u(t) \end{bmatrix}^T \right)^{-1}$$

There are ways of constructing $\tilde{x}(t)$ from input-output data (*direct N4SID*).

- If the (extended) observability matrix Γ_r is known, (A, C) can be extracted. Since

$$y(t) = C(qI - A)^{-1} Bu(t) + Du(t) + \tilde{e}(t)$$

(B, D) can also be determined.

$$\Gamma_r = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{r-1} \end{bmatrix}$$

There are many ways of constructing Γ_r (or some similar matrix) from input-output data (*realization-based N4SID methods*).

Basic Idea of Subspace Identification

- One way is as follows (basically according to Ljung, 1999):

$$\mathbf{Y}_{0|-s_1} = \begin{bmatrix} y(0) & \cdots & y(N-1) \\ \vdots & \ddots & \vdots \\ y(-s_1) & \cdots & y(N-1-s_1) \end{bmatrix}, \quad \mathbf{U}_{0|-s_2} = \begin{bmatrix} u(0) & \cdots & u(N-1) \\ \vdots & \ddots & \vdots \\ u(-s_2) & \cdots & u(N-1-s_2) \end{bmatrix}$$

$$\Phi = \begin{bmatrix} \mathbf{Y}_{0|-s_1} \\ \mathbf{U}_{0|-s_2} \end{bmatrix}, \quad G = \frac{1}{N} \mathbf{Y}_{1|r} \left[\mathbf{I} - \mathbf{U}_{1|r}^T (\mathbf{U}_{1|r} \mathbf{U}_{1|r}^T)^{-1} \mathbf{U}_{1|r} \right] \Phi^T$$

$$\hat{G} = W_1 G W_2 = USV^T \approx U_1 S_1 V_1^T, \quad \hat{\Gamma}_r = W_1^{-1} U_1 R$$

W_1 , W_2 and R are weighting matrices given by the particular method.

- S_1 is a matrix of singular values obtained by **omitting the insignificant singular values** from S (note that data are corrupted by noise). In principle, this is a **user choice**.
- ***Is this a problem for identification of ill-conditioned MIMO systems, where small singular values in the gain matrix are very relevant?***

Design of Identification Experiments

Preliminary analysis

- ◆ It is desirable to make the identification (equally) **informative for all** relevant “directions”
- ◆ Consider a **singular value decomposition** of the gain matrix, i.e.

$$y = Gu = U\Sigma V^T u = \sum_{i=1}^n U_i \sigma_i V_i^T u$$

- the input $u = u^i = V_i \sigma_i^{-1}$ will produce the output $y = y^i = U_i$, $\|y^i\| = 1$
- ◆ To properly excite all directions i , $i = 1, \dots, n$, we need to apply **inputs** u^i that **vary** (symmetrically) **between**

$$u_-^i = -\sigma_i^{-1} V_i \quad \text{and} \quad u_+^i = +\sigma_i^{-1} V_i$$

- it is sufficient to know σ_i (a scalar) approximately; V_i may have to be more accurately estimated (but not difficult for distillation)

Design of Identification Experiments

Some design options

- ◆ Excitation of **one direction at a time**
 - the input u is varied between u_-^1 and u_+^1 in one part of the experiment, between u_-^2 and u_+^2 in another part, etc.
- ◆ Excitation of **all directions simultaneously**
 - the input u is given by $u = \frac{1}{n} \sum_{i=1}^n u^i$, where the u^i :s are varied simultaneously in an uncorrelated way
- ◆ **Note 1:** The above principles apply **irrespective of what type of signal** is used to move u^i between u_-^i and u_+^i (e.g., PRBS).
- ◆ **Note 2:** Perturbation of the inputs one at a time or simultaneously in uncorrelated ways are generally **not optimal** designs.

Application to Distillation



N4SID identification

- How sensitive is it to the experimental design?
- Is the choice of order a problem (in MATLAB's System Identification Toolbox)?
- How to handle time delays?

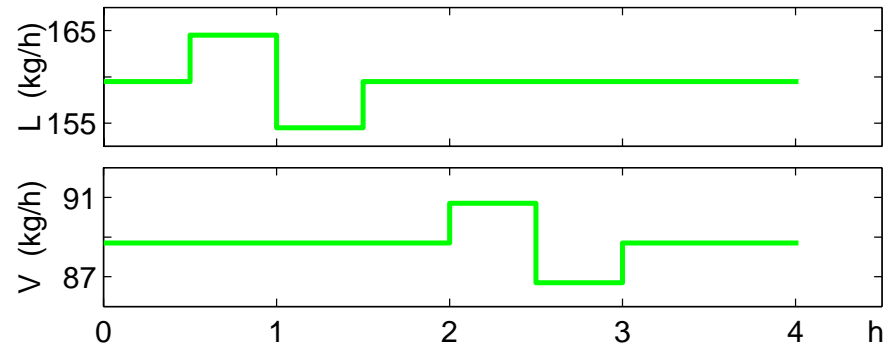
$$x(k+1) = Ax(k) + B \begin{bmatrix} u_1(k - \theta_1) \\ u_2(k - \theta_2) \end{bmatrix}$$

$$\begin{bmatrix} y_1(k) \\ y_2(k + \theta_3) \end{bmatrix} = Cx(k)$$

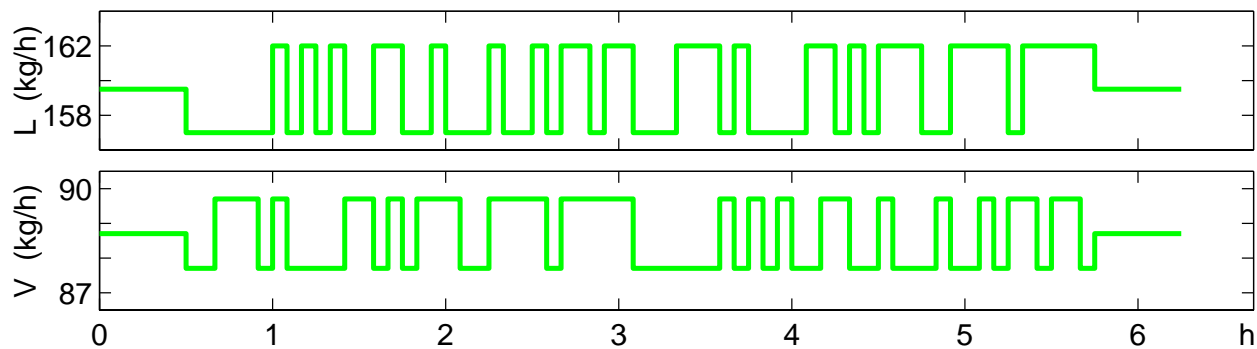
Pilot-scale distillation column at Åbo Akademi University

Identification experiments

- ◆ Step changes of inputs one at a time (**SeqStep**)

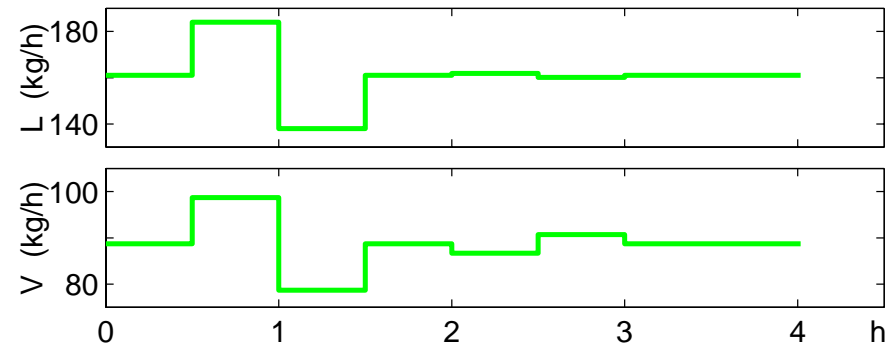


- ◆ Simultaneous uncorrelated PRBS in inputs (**UncPRBS**)

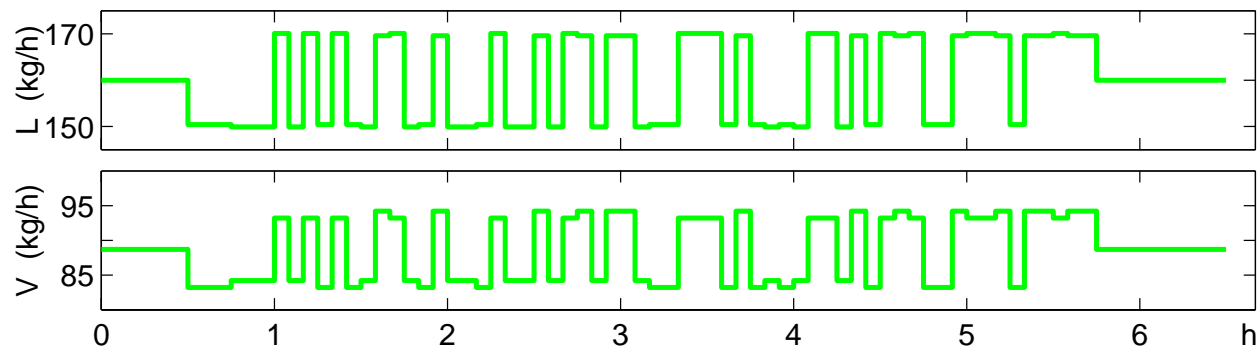


— Identification experiments

◆ Step changes in gain directions (**DirStep**)



◆ Simultaneous PRBS excitation of gain directions (**SimDirPRBS**)



N4SID Identification

◆ Step changes of inputs one at a time (SeqStep)

- Default order (figure)

$$\theta_1 = \theta_2 = 6, \theta_3 = 12$$

$$n = 3, \bar{e}^2 = 6.79 \times 10^{-7}$$

$$\sigma(A) = 1.00, 0.99, 0.81$$

$$\sigma(K) = 0.784, 0.002$$

- Fix order = 3

$$\bar{e}^2 = 5.79 \times 10^{-7} \quad !!$$

$$\sigma(A) = 1.00, 0.96, 0.34$$

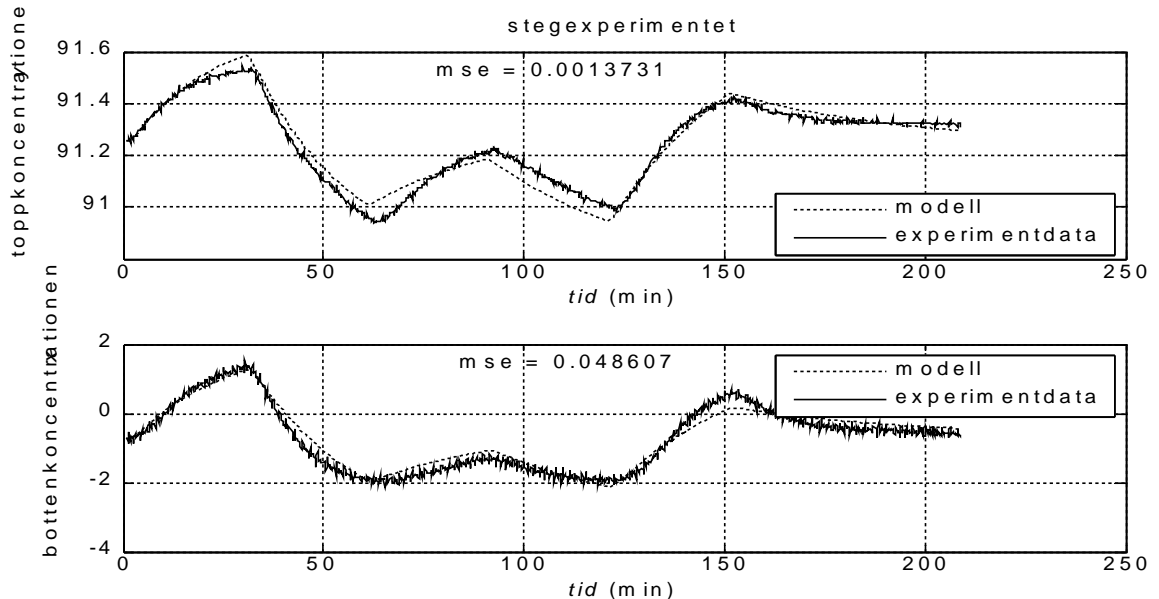
$$\sigma(K) = 1.161, 0.028 \quad !$$

- Better order = 4 (?)

$$\bar{e}^2 = 4.65 \times 10^{-7}$$

$$\sigma(A) = 1.05, 1.00, 0.99, 0.23$$

$$\sigma(K) = 5.007, 0.036$$



- Better time delays: $\theta_1 = 12, \theta_2 = 15, \theta_3 = 9$ (?)

$$n = 4, \bar{e}^2 = 3.60 \times 10^{-7}$$

$$\sigma(A) = 1.05, 1.00, 0.99, 0.28 \quad (\text{consistent } \sigma(A)!)$$

$$\sigma(K) = 0.467, 0.114 \quad (\text{inconsistent } \sigma(K))$$

— N4SID identification

◆ Simultaneous uncorrelated PRBS (**UncPRBS**)

- Default order (figure)

$$\theta_1 = \theta_2 = 6, \theta_3 = 12$$

$$n = 4, \bar{e}^2 = 7.78 \times 10^{-8}$$

$$\sigma(A) = 1.00, 0.99, 0.95, 0.26$$

$$\sigma(K) = 0.777, 0.001$$

- Fix order = 4

$$\bar{e}^2 = 8.61 \times 10^{-8} !$$

$$\sigma(A) = 1.18, 1.00, 0.99, 0.08$$

$$\sigma(K) = 0.550, 0.003$$

- Better order = 5 (?)

$$\bar{e}^2 = 5.22 \times 10^{-8}$$

$$\sigma(A) = 1.04, 1.00, 0.99, 0.81, 0.63$$

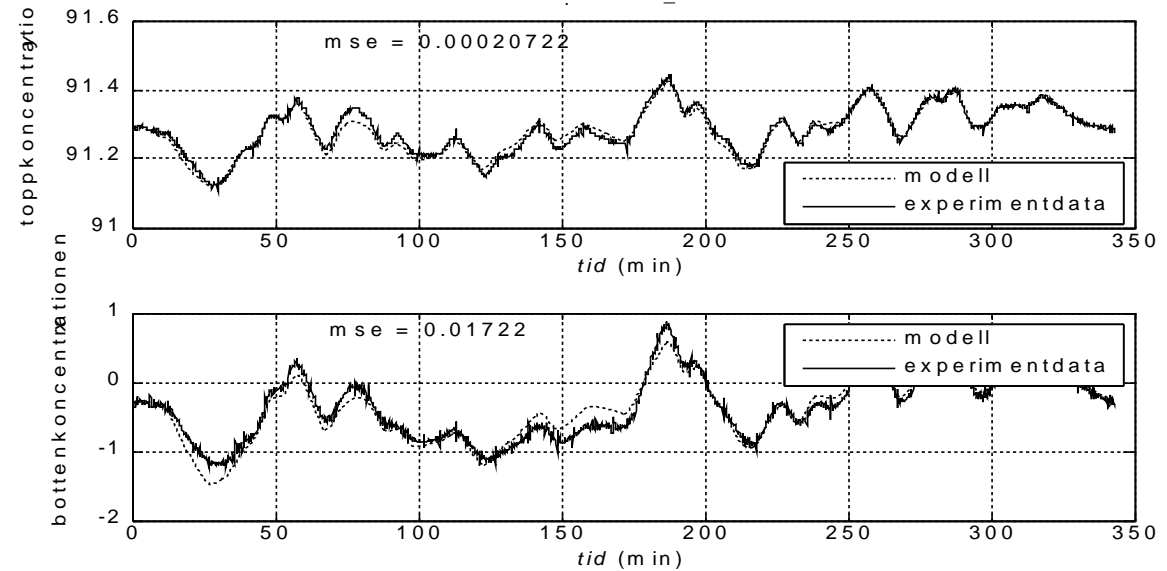
$$\sigma(K) = 0.770, 0.003$$

- Better time delays: $\theta_1 = 12, \theta_2 = 15, \theta_3 = 9$ (??)

$$n = 4, \bar{e}^2 = 7.49 \times 10^{-8}$$

$$\sigma(A) = 1.00, 0.99, 0.97, 0.23$$

$$\sigma(K) = 0.803, 0.000001 !!!$$



— N4SID identification

◆ Simultaneous PRBS in gain directions (**SimDirPRBS**)

– Default order (figure)

$$\theta_1 = \theta_2 = 6, \theta_3 = 12$$

$$n = 3, \bar{e}^2 = 6.73 \times 10^{-8}$$

$$\sigma(A) = 1.00, 0.99, 0.92$$

$$\sigma(K) = 1.387, 0.013$$

– Fix order = 3

$$\bar{e}^2 = 8.44 \times 10^{-8} \quad !!$$

$$\sigma(A) = 1.00, 0.99, 0.43$$

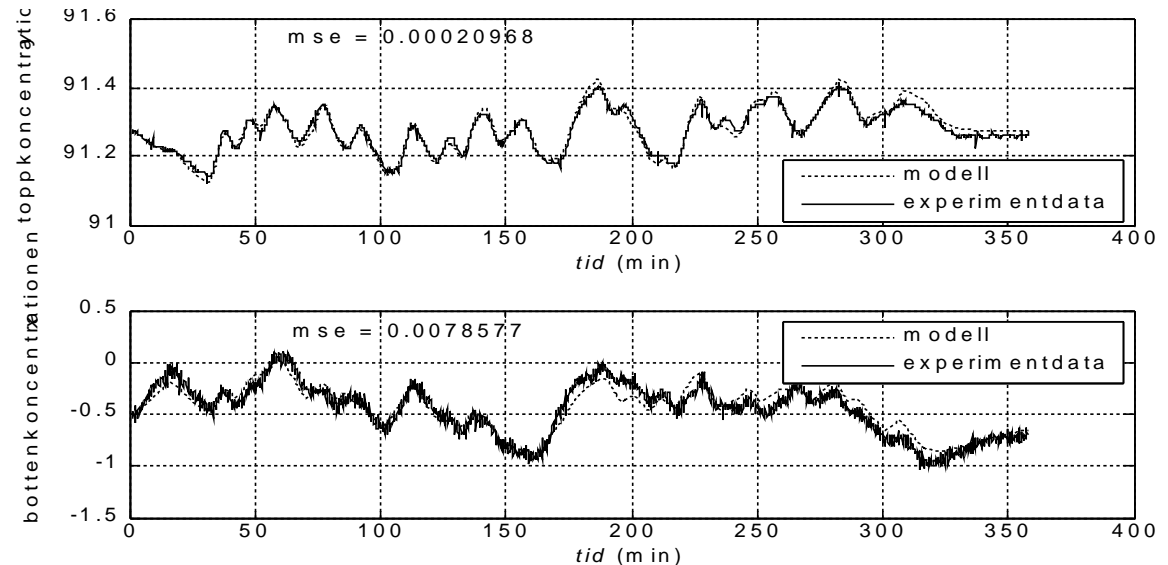
$$\sigma(K) = 1.220, 0.023$$

– Better order = 4 (??)

$$\bar{e}^2 = 9.92 \times 10^{-8} \quad !!$$

$$\sigma(A) = 1.41, 1.00, 0.99, 0.19$$

$$\sigma(K) = 1.318, 0.019$$



– Better time delays: $\theta_1 = 12, \theta_2 = 15, \theta_3 = 9$

$$n = 4, \bar{e}^2 = 5.10 \times 10^{-8} \quad (n = 4 \text{ is default choice!})$$

$$\sigma(A) = 1.01, 0.99, 0.98, 0.30$$

$$\sigma(K) = 1.221, 0.014 \quad (\text{very consistent } \sigma(K))$$

— N4SID identification

◆ Step changes in gain directions (**DirStep**)

– Default order (figure)

$$\theta_1 = \theta_2 = 6, \theta_3 = 12$$

$$n = 4, \bar{e}^2 = 1.33 \times 10^{-7}$$

$$\sigma(A) = 1.09, 0.99, 0.98, 0.24$$

$$\sigma(K) = 1.459, 0.013$$

– Fix order = 4

$$\bar{e}^2 = 1.43 \times 10^{-7} \quad !!$$

$$\sigma(A) = 1.44, 0.99, 0.99, 0.03 \quad !$$

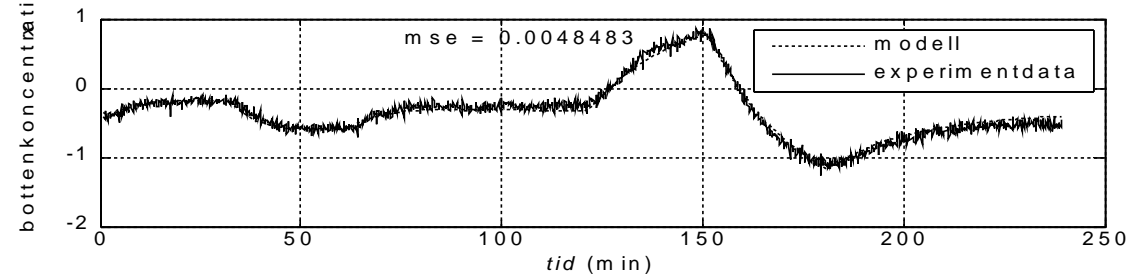
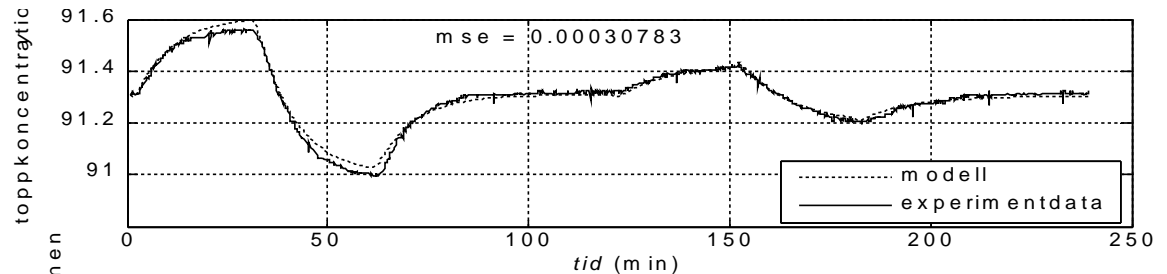
$$\sigma(K) = 1.532, 0.014$$

– Better order = 3 (???)

$$\bar{e}^2 = 1.21 \times 10^{-7} \quad !!$$

$$\sigma(A) = 0.99, 0.99, 0.40$$

$$\sigma(K) = 1.558, 0.015$$



– Better time delays: $\theta_1 = 12, \theta_2 = 15, \theta_3 = 9$ (?)

$$n = 4, \bar{e}^2 = 1.04 \times 10^{-7}$$

$$\sigma(A) = 1.00, 0.99, 0.98, 0.06 \quad !!$$

$$\sigma(K) = 1.453, 0.013 \quad (\text{very consistent } \sigma(K))$$

Conclusions

- ◆ Some observations about the N4SID algorithm:
 - The “loss function” (\sim variance of the disturbance model) does not always decrease with increasing model order.
 - The default choice of model order does not always seem “right”.
 - Fixing the model order to the default order changes the loss function and can dramatically change estimated parameters (maybe different weight matrices are used?).
- ◆ Some other observations:
 - Consistent gain estimates require experiments that properly excite the “gain directions”.
 - A good choice of time delays is a demanding task.